

simulations of coupled mechanics and transport in growing soft tissue

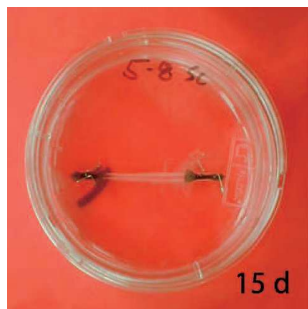
H. Narayanan, K. Garikipati, E. M. Arruda & K. Grosh
University of Michigan

third M.I.T conference on computational fluid and solid mechanics

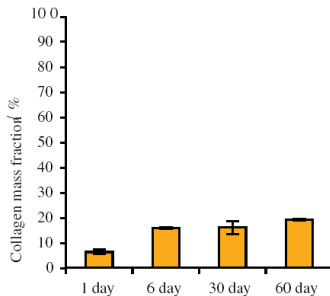
June 14th, 2005 – Cambridge, MA

motivation and definition

growth/resorption – an addition or loss of mass



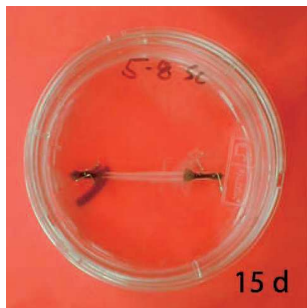
engineered tendon constructs [Calve et al, 2004]



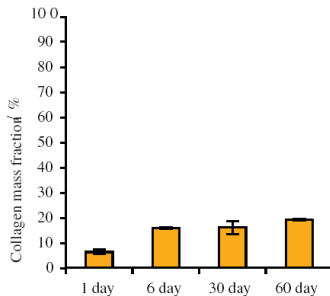
increasing collagen concentration with age

motivation and definition

growth/resorption – an addition or loss of mass



engineered tendon constructs [Calve et al, 2004]



increasing collagen concentration with age

open system with multiple species inter-converting and interacting

modelling approach

classical balance laws enhanced via fluxes and sources

- solid – collagen, proteoglycans, cells
- extra cellular fluid
 - undergoes transport relative to the solid phase
- dissolved solutes (sugars, proteins, ...)
 - undergo transport relative to fluid

modelling approach

classical balance laws enhanced via fluxes and sources

- solid – collagen, proteoglycans, cells
- extra cellular fluid
 - undergoes transport relative to the solid phase
- dissolved solutes (sugars, proteins, . . .)
 - undergo transport relative to fluid

modelling approach

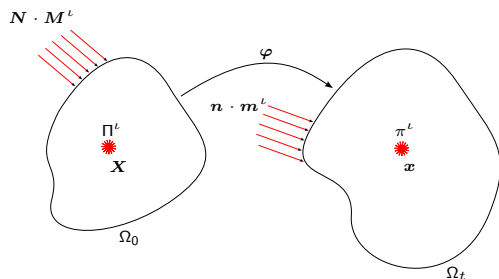
classical balance laws enhanced via fluxes and sources

- solid – collagen, proteoglycans, cells
- extra cellular fluid
 - undergoes transport relative to the solid phase
- dissolved solutes (sugars, proteins, . . .)
 - undergo transport relative to fluid

brief subset of related literature:

- Cowin and Hegedus [1976]
- Kuhl and Steinmann [2002]
- Sengers, Oomens and Baaijens [2004]
- *Garikipati et al. – journal of the mechanics and physics of solids (52) 1595-1625 [2004]*

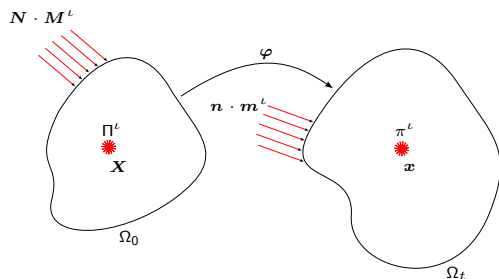
balance of mass



ρ_0^l – species concentration
 Π^l – species production
 M^l – species flux

- for a species:
$$\frac{\partial \rho_0^l}{\partial t} = \Pi^l - \nabla_X \cdot M^l$$
- solid – no flux; no boundary conditions
- fluid – no source; concentration or flux boundary conditions
- solute – flux and source; concentration boundary condition

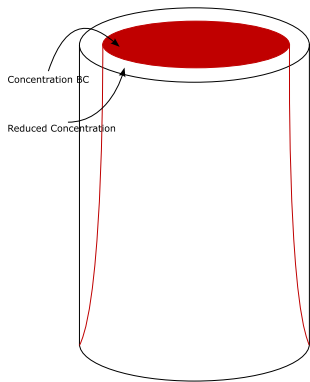
balance of mass



ρ_0^l – species concentration
 Π^l – species production
 M^l – species flux

- for a species:
$$\frac{\partial \rho_0^l}{\partial t} = \Pi^l - \nabla_X \cdot M^l$$
- solid – no flux; no boundary conditions
- fluid – no source; concentration or flux boundary conditions
- solute – flux and source; concentration boundary condition

configuration and physical boundary conditions



boundary condition specification

$$\frac{d\rho^i}{dt} + \rho^i \nabla_x \cdot \mathbf{v} = -\nabla_x \cdot \mathbf{m}^i + \pi^i$$

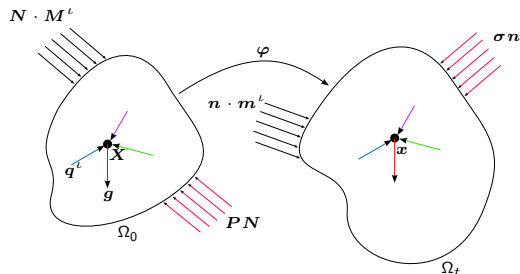
ρ^i – current species concentration

π^i – current species production

\mathbf{m}^i – current species flux

\mathbf{v} – solid velocity

balance of momentum



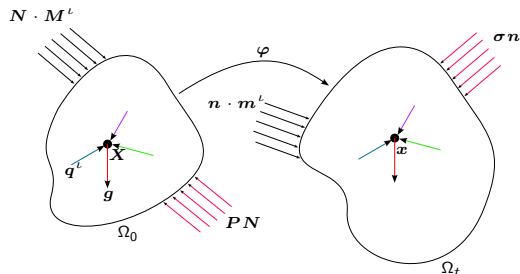
ρ_0^l – species concentration
 \mathbf{V} – solid velocity
 \mathbf{V}^l – species relative velocity
 \mathbf{g} – body force
 \mathbf{q}^l – interaction force
 \mathbf{P}^l – partial stress

- for a species, velocity relative to the solid: $\mathbf{V}^l = (1/\rho_0^l)\mathbf{F}\mathbf{M}^l$

$$\rho_0^l \frac{\partial}{\partial t} (\mathbf{V} + \mathbf{V}^l) = \rho_0^l (\mathbf{g} + \mathbf{q}^l) + \nabla_{\mathbf{X}} \cdot \mathbf{P}^l - (\nabla_{\mathbf{X}} (\mathbf{V} + \mathbf{V}^l)) \mathbf{M}^l$$

- negligible contribution to mechanics from dissolved solutes

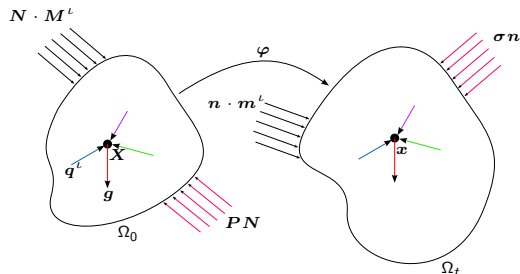
balance of momentum



ρ_0^l – species concentration
 \mathbf{V} – solid velocity
 \mathbf{V}^l – species relative velocity
 \mathbf{g} – body force
 \mathbf{q}^l – interaction force
 \mathbf{P}^l – partial stress

- for a species, velocity relative to the solid: $\mathbf{V}^l = (1/\rho_0^l)\mathbf{F}\mathbf{M}^l$
$$\rho_0^l \frac{\partial}{\partial t} (\mathbf{V} + \mathbf{V}^l) = \rho_0^l (\mathbf{g} + \mathbf{q}^l) + \nabla_X \cdot \mathbf{P}^l - (\nabla_X (\mathbf{V} + \mathbf{V}^l)) \mathbf{M}^l$$
- negligible contribution to mechanics from dissolved solutes

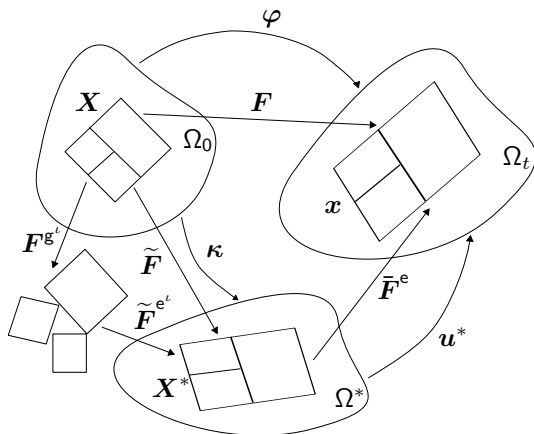
balance of momentum



ρ_0^l – species concentration
 \mathbf{V} – solid velocity
 \mathbf{V}^l – species relative velocity
 \mathbf{g} – body force
 \mathbf{q}^l – interaction force
 \mathbf{P}^l – partial stress

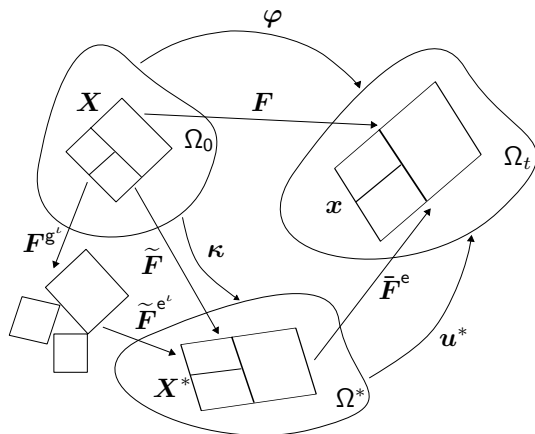
- for a species, velocity relative to the solid: $\mathbf{V}^l = (1/\rho_0^l)\mathbf{F}\mathbf{M}^l$
 $\rho_0^l \frac{\partial}{\partial t} (\mathbf{V} + \mathbf{V}^l) = \rho_0^l (\mathbf{g} + \mathbf{q}^l) + \nabla_X \cdot \mathbf{P}^l - (\nabla_X (\mathbf{V} + \mathbf{V}^l)) \mathbf{M}^l$
- negligible contribution to mechanics from dissolved solutes

growth kinematics



- $F = \bar{F}^e \tilde{F}^{e^l} F^{g^l}$; $F^{e^l} = \bar{F}^e \tilde{F}^{e^l}$; internal stress due to \tilde{F}^{e^l}
- isotropic swelling due to growth: $F^{g^l} = \frac{\rho_0}{\rho_{0_{int}}} \mathbf{1}$
- saturation and swelling

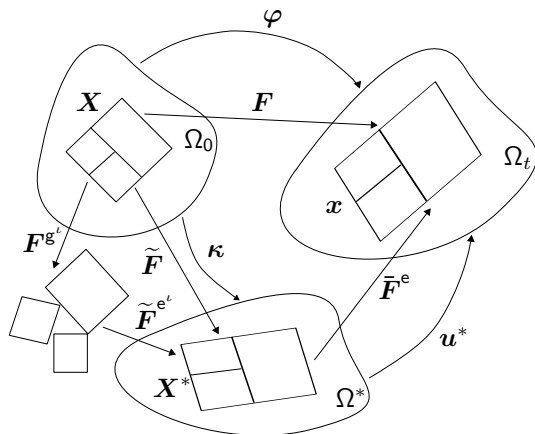
growth kinematics



- $F = \bar{F}^e \tilde{F}^{e^l} F^{g^l}$; $F^{e^l} = \bar{F}^e \tilde{F}^{e^l}$; internal stress due to \tilde{F}^{e^l}
- isotropic swelling due to growth: $F^{g^l} = \frac{\rho_0^l}{\rho_{0_{ini}}^l} \mathbf{1}$

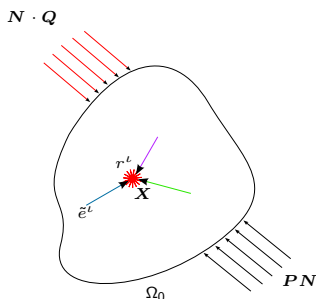
• saturation and swelling

growth kinematics



- $F = \bar{F}^e \tilde{F}^{e^l} F^{g^t}$; $F^{e^l} = \bar{F}^e \tilde{F}^{e^l}$; internal stress due to \tilde{F}^{e^l}
- isotropic swelling due to growth: $F^{g^t} = \frac{\rho_0^l}{\rho_{0_{ini}}^l} \mathbf{1}$
- saturation and swelling

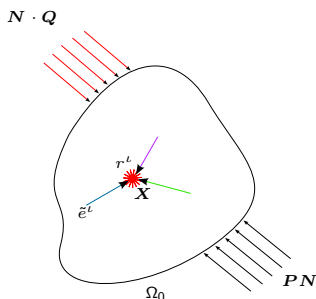
energy balance and entropy inequality



- ρ_0^ℓ – species concentration
- e^ℓ – specific internal energy
- P^ℓ – partial stress
- F – deformation gradient
- V^ℓ – species relative velocity
- Q^ℓ – partial heat flux
- r^ℓ – species heat supply
- \tilde{e}^ℓ – energy transfer
- M^ℓ – species flux

$$\rho_0^\ell \frac{\partial e^\ell}{\partial t} = P^\ell : \dot{F} + P^\ell : \nabla_X V^\ell - \nabla_X \cdot Q^\ell + r^\ell + \rho_0^\ell \tilde{e}^\ell - \nabla_X e^\ell \cdot (M^\ell)$$

energy balance and entropy inequality



- ρ_0^ℓ – species concentration
- e^ℓ – specific internal energy
- \mathbf{P}^ℓ – partial stress
- \mathbf{F} – deformation gradient
- \mathbf{V}^ℓ – species relative velocity
- \mathbf{Q}^ℓ – partial heat flux
- r^ℓ – species heat supply
- \tilde{e}^ℓ – energy transfer
- \mathbf{M}^ℓ – species flux
- η^ℓ – species entropy
- θ – temperature

$$\rho_0^\ell \frac{\partial e^\ell}{\partial t} = \mathbf{P}^\ell : \dot{\mathbf{F}} + \mathbf{P}^\ell : \nabla_X \mathbf{V}^\ell - \nabla_X \cdot \mathbf{Q}^\ell + r^\ell + \rho_0^\ell \tilde{e}^\ell - \nabla_X e^\ell \cdot (\mathbf{M}^\ell)$$

$$\sum_{\ell=\alpha}^{\omega} \rho_0^\ell \frac{\partial \eta^\ell}{\partial t} \geq \sum_{\ell=\alpha}^{\omega} \left(\frac{r^\ell}{\theta} - \nabla_X \eta^\ell \cdot \mathbf{M}^\ell - \frac{\nabla_X \cdot \mathbf{Q}^\ell}{\theta} + \frac{\nabla_X \theta \cdot \mathbf{Q}^\ell}{\theta^2} \right)$$

constitutive relations for fluxes

- combine first and second laws to get dissipation inequality
- constitutive hypothesis $e^l = \hat{e}^l(\mathbf{F}^{e^l}, \rho_0^l, \eta^l)$
 \Rightarrow consistent constitutive relations

- fluid flux relative to collagen

$$\mathbf{M}^f = \mathbf{D}^f \left(\rho_0^f \mathbf{F}^{T^f} \mathbf{g} + \mathbf{F}^{T^f} \nabla_{\mathbf{X}} \cdot \mathbf{P}^f - \nabla_{\mathbf{X}} (e^f - \theta \eta^f) \right)$$

- solute flux (proteins, sugars, nutrients, ...) relative to fluid

$$\tilde{\mathbf{V}}^s = \mathbf{V}^s - \mathbf{V}^f$$

$$\tilde{\mathbf{M}}^s = \mathbf{D}^s \left(-\nabla_{\mathbf{X}} (e^s - \theta \eta^s) \right)$$

- \mathbf{D}^f and \mathbf{D}^s – positive semi-definite mobility tensors
magnitudes from literature, e.g. Mauck et al. [2003]

constitutive relations for fluxes

- combine first and second laws to get dissipation inequality
- constitutive hypothesis $e^l = \hat{e}^l(\mathbf{F}^{e^l}, \rho_0^l, \eta^l)$
 \Rightarrow consistent constitutive relations
- fluid flux relative to collagen

$$\mathbf{M}^f = \mathbf{D}^f \left(\rho_0^f \mathbf{F}^T \mathbf{g} + \mathbf{F}^T \nabla_X \cdot \mathbf{P}^f - \nabla_X (e^f - \theta \eta^f) \right)$$

- solute flux (proteins, sugars, nutrients, ...) relative to fluid

$$\tilde{\mathbf{V}}^s = \mathbf{V}^s - \mathbf{V}^f$$

$$\tilde{\mathbf{M}}^s = \mathbf{D}^s \left(-\nabla_X (e^s - \theta \eta^s) \right)$$

- \mathbf{D}^f and \mathbf{D}^s – positive semi-definite mobility tensors
magnitudes from literature, e.g. Mauck et al. [2003]

constitutive relations for fluxes

- combine first and second laws to get dissipation inequality
- constitutive hypothesis $e^l = \hat{e}^l(\mathbf{F}^{e^l}, \rho_0^l, \eta^l)$
 \Rightarrow consistent constitutive relations

- fluid flux relative to collagen

$$\mathbf{M}^f = \mathbf{D}^f \left(\rho_0^f \mathbf{F}^T \mathbf{g} + \mathbf{F}^T \nabla_X \cdot \mathbf{P}^f - \nabla_X (e^f - \theta \eta^f) \right)$$

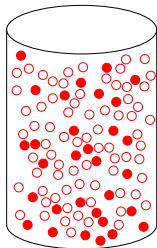
- solute flux (proteins, sugars, nutrients, ...) relative to fluid

$$\tilde{\mathbf{V}}^s = \mathbf{V}^s - \mathbf{V}^f$$

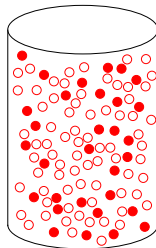
$$\tilde{\mathbf{M}}^s = \mathbf{D}^s (-\nabla_X (e^s - \theta \eta^s))$$

- \mathbf{D}^f and \mathbf{D}^s – positive semi-definite mobility tensors
magnitudes from literature, e.g. Mauck et al. [2003]

saturation and Fickian diffusion



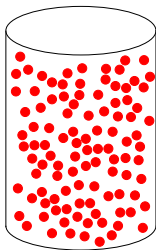
configuration 1



configuration 2

- change in configurational entropy with distribution of solute particles ... **if** solvent is not saturated with solute

saturation and Fickian diffusion

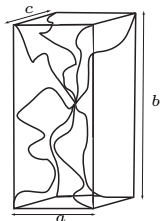


only possible configuration

- saturated \Rightarrow single configuration \Rightarrow no Fickian diffusion
- still have concentration-gradient driven transport due to stress gradient contribution to flux

worm-like chain model based internal energy density

$$\tilde{\rho}_0^c \hat{e}^c(\mathbf{F}^{e^c}, \rho_0^c)$$



$$\begin{aligned}
 &= \frac{Nk\theta}{4A} \left(\frac{r^2}{2L} + \frac{L}{4(1-r/L)} - \frac{r}{4} \right) \\
 &- \frac{Nk\theta}{4\sqrt{2L/A}} \left(\sqrt{\frac{2A}{L}} + \frac{1}{4(1-\sqrt{2A/L})} - \frac{1}{4} \right) \log(\lambda_1^{a^2} \lambda_2^{b^2} \lambda_3^{c^2}) \\
 &+ \frac{\gamma}{\beta} (J^{e^c} - 1) + 2\gamma \mathbf{1} : \mathbf{E}^{e^c}
 \end{aligned}$$

- embed in multi chain model [Bischoff et al., 2002]

$$r = \frac{1}{2} \sqrt{a^2 \lambda_1^{e^2} + b^2 \lambda_2^{e^2} + c^2 \lambda_3^{e^2}}$$

- λ_I^e – elastic stretches along a, b, c
- $$\lambda_I^e = \sqrt{\mathbf{N}_I \cdot \mathbf{C}^e \mathbf{N}_I}$$

some possibilities for sources

- simple first order rate law
 - constituents either “solid” or “fluid”

$$\Pi^f = -k^f(\rho_0^f - \rho_{0ini}^f), \quad \Pi^c = -\Pi^f$$

- strain energy dependencies
 - weighted by relative densities

some possibilities for sources

- simple first order rate law
 - constituents either “solid” or “fluid”

$$\Pi^f = -k^f(\rho_0^f - \rho_{0ini}^f), \quad \Pi^c = -\Pi^f$$

- strain energy dependencies
 - weighted by relative densities

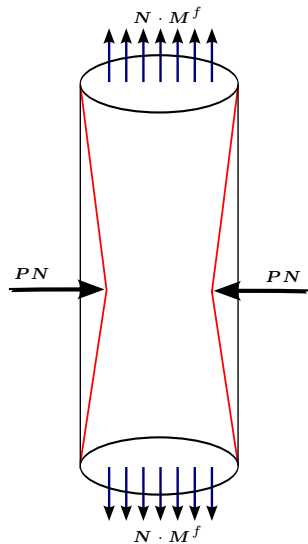
$$\Pi^c = \left(\frac{\rho_0^c}{\rho_{0ini}^c}\right)^{-m} \Psi_0 - \Psi_0^*$$

Harrigan & Hamilton [1993]

computational formulation details

- implementation in FEAP
- coupled implementation; staggered scheme (Armero [1999], Garikipati et al. [2001])
- nonlinear projection methods to treat incompressibility (Simo et al. [1985])
- energy-momentum conserving algorithm for dynamics (Simo & Tarnow [1992a,b])
- backward Euler for time-dependent mass balance
- mixed method for stress/strain gradient-driven fluxes (Garikipati et al. [2001])
- large advective terms require stabilization

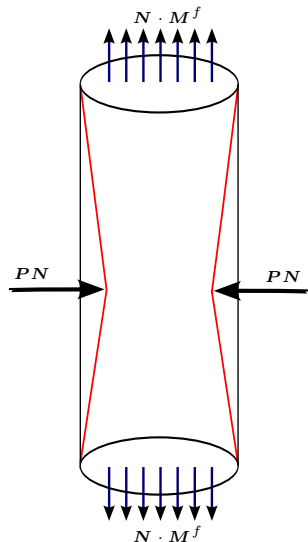
examples of coupled computation – constriction



- simulating a tendon immersed in a bath
- constrict it to force fluid and dissolved nutrient flow \Rightarrow guided tendon growth
- biphasic model

- fluid mobility $D_{ij}^f = 1 \times 10^{-8} \delta_{ij}$, Han et al. [2000]
- first order rate law:
 $\Gamma^f = -k^f(\rho^f - \rho_{0,mi}^f)$, $\Gamma^c = -\Gamma^f$

examples of coupled computation – constriction

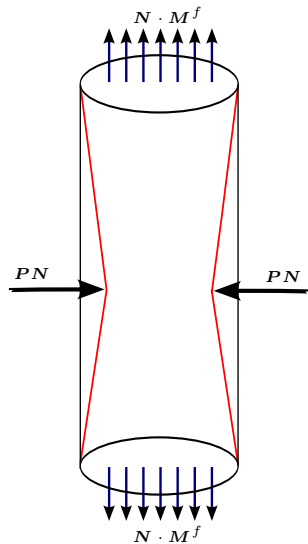


- simulating a tendon immersed in a bath
- constrict it to force fluid and dissolved nutrient flow \Rightarrow guided tendon growth
- biphasic model
 - worm-like chain model for collagen
 - ideal nearly incompressible fluid
- fluid mobility $D_{ij}^f = 1 \times 10^{-8} \delta_{ij}$, Han et al. [2000]

• first order rate law:

$$\Gamma^f = -k^f (\rho^f - \rho_{0m}^f), \quad \Gamma^c = -\Gamma^f$$

examples of coupled computation – constriction



- simulating a tendon immersed in a bath
- constrict it to force fluid and dissolved nutrient flow \Rightarrow guided tendon growth
- biphasic model
 - worm-like chain model for collagen
 - ideal nearly incompressible fluid
$$\rho^f \hat{e}^f = \frac{1}{2} \kappa (\det(\mathbf{F}^{e^f}) - 1)^2$$
- fluid mobility $D_{ij}^f = 1 \times 10^{-8} \delta_{ij}$, Han et al. [2000]
- first order rate law:
$$\Pi^f = -k^f (\rho^f - \rho_{0ini}^f), \quad \Pi^c = -\Pi^f$$

results and inferences

- total flux in the vertical direction
- stress driven diffusion

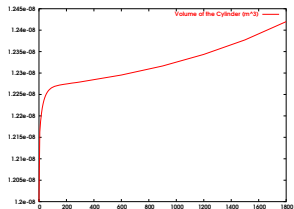
results and inferences

- regions of high fluid concentration
⇒ faster growth
- relaxation after constriction concludes

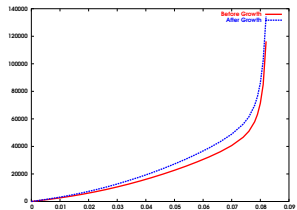
swelling of a tendon immersed in a bath

collagen concentration evolution

volume evolution curve



stress-extension curves



summary and further work

- physiologically relevant continuum formulation describing growth in an open system – consistent with mixture theory
- relevant driving forces arise from thermodynamics – coupling with mechanics
- gained insights into the problem
 - issues of saturation and growth
 - saturation and Fickian diffusion
 - configurations and physical boundary conditions
- more careful treatment of biochemistry – nature of sources
- formulated a theoretical framework for remodelling
- engineering and characterization of growing, functional biological tissue to drive and validate modelling

summary and further work

- physiologically relevant continuum formulation describing growth in an open system – consistent with mixture theory
- relevant driving forces arise from thermodynamics – coupling with mechanics
- gained insights into the problem
 - issues of saturation and growth
 - saturation and Fickian diffusion
 - configurations and physical boundary conditions
- more careful treatment of biochemistry – nature of sources
- formulated a theoretical framework for remodelling
- engineering and characterization of growing, functional biological tissue to drive and validate modelling

summary and further work

- physiologically relevant continuum formulation describing growth in an open system – consistent with mixture theory
- relevant driving forces arise from thermodynamics – coupling with mechanics
- gained insights into the problem
 - issues of saturation and growth
 - saturation and Fickian diffusion
 - configurations and physical boundary conditions
- more careful treatment of biochemistry – nature of sources
- formulated a theoretical framework for remodelling
- engineering and characterization of growing, functional biological tissue to drive and validate modelling